

Hardness and Tensile Properties of Prophylactic Knee Brace Produced from Cow Bone and Periwinkle Shell Composites

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ABSTRACT

Application of reinforced aluminium scrap for the production of prophylactic knee brace (Pkb) particularly with agro-waste materials is rarely available. In this work, hardness and tensile properties of aluminium alloy (Al 6063) straps reinforced with cow bone (Cb) and periwinkle shell (Ps) for the production of Pkb were investigated. The Cb and Ps sourced were cleaned and the Cb was sun-dried for 4 weeks before crushing with Denver laboratory Ball mill (Model: 48-D0500/Q). The Ps was also crushed, sun-dried for 7 days and treated in the oven (Model SDO/225) at 110 °C for 30 minutes to remove moisture. The particle size of 75 μm was used to cast six (6) each of aluminium/cowbone (Al/Cb) and aluminium/periwinkle shell (Al/Ps) composites. The cast aluminium composites of Pkb and original Pkb were investigated for density, hardness, and tensile properties. It was observed that addition of Cb and Ps in the cast Pkb gave a density of 2.68 g/cm³ and 2.60 g/cm³ respectively. The average values of hardness and tensile strength obtained were 41.18 BHN and 135.88 MPa respectively when Ps was added to the cast aluminium Pkb, while addition of Cb gave harness values of 40.45 BHN and tensile strength of 134.63 MPa.

Keywords: Turning, Coolant temperature, Ti6Al4V, Surface roughness, Machining Parameter

1 INTRODUCTION

The rate of wastes generation in modern day life has tremendously increased in which its composition and the magnitude generated have influence on the way the population lives [1]. Improper management of such wastes may have been accountable for degrading the environmental and the difficulty in its disposal [1, 2]. This work focused on using aluminium alloy (Al 6063) straps that is the off-cut generated from the production of aluminium doors and windows. The aluminium alloy off-cut was used as matrix while periwinkle shell (Ps) and cowbone (Cb) were used as reinforcements to form a composite for the production of prophylactic knee brace (Pkb) used in bone support. Pkb consists of the brace (metal), hinge (link point) and strap system. Pkb is usually used as components for knee injury management (preventive and healing mechanism) of knee injuries [3, 4].

Many works on reinforcement of aluminium have been carried out [5-12]. Among these, Umunakwe et al. [12] reported on mechanical properties and microstructures of Particulate Periwinkle Shell-aluminium 6063 Metal Matrix Composite (PPS-AIMMC) and comparing the properties of the composites with those of the aluminium 6063 (AA6063) alloy. Application of aluminium scrap for Pkb particularly with Ps and Cb as reinforcements is rarely available. The focus of this study is to investigate the hardness and tensile properties of Prophylactic Knee Brace Produced from Cow bone and Periwinkle Shell Composites

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2 MATERIALS AND METHODS

The materials used are: The off-cut (scraps) of Aluminium (Al 6063) (door and window frames) produced by Nigeria Aluminium Extrusions Limited, Lagos Nigeria. The Ps and Cb were sourced from river bank and abattoir respectively.

2.1 PREPARATION OF SAMPLES

2.1.1 Preparation of Aluminium Scrap

The aluminium scraps were cleaned and sun dried for 24 hours to remove dirt before charged into furnace (Model No. M254 and Serial No. AD3246P) for melting and de-slagging. The molten aluminium was stirred and cast into a rectangular bar. The solidified material was reduced to smaller sizes. The percentage composition of the aluminium alloy used is shown in (Table 1)

Table 1: Chemical composition of aluminium (Al 6063) off-cut [12]

Element	Al	Si	Fe	Cu	Mn	Mg	Zn	Cr	Ti	Ca	Other
Wt %	98.18	0.60	0.46	0.012	0.024	0.35	<0.002	0.01	0.06	0.07	0.12

2.1.2 Preparation of Periwinkle Shell (Ps)

The Ps (Figure 1) were cleansed by soaking for 24 hours, boiled in water and detergent at 100 °C for 50 minutes and cooled in air. The washing was carried out by wire brush to remove sand particles and dirt. It was later reduced into smaller sizes and sun dried for 7 days. The Ps was heated in an oven (Model SDO/225 Serial No. Y9C227) at 110 °C for 30 minutes to remove moisture as reported by Umunakwe et al., [12]. The chemical composition of Ps powder as used by Nwabufor [13] (Table 2). The Ps was crushed with Denver laboratory ball mill (Model 48-D0500/0 with Serial No. 14002201). Pulverized and sieved to 75µm particle size using BS standard sieves (Figure 2).



Figure 1: Periwinkle Shells (Ps)



Figure 2: Pulverized Periwinkle Shell

Table 2: Chemical composition of periwinkle shell powder [13].

Constitute	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	SO ₃	K ₂ O	Na ₂ O	Mn ₂ O ₃	P ₂ O	TiO ₂
Composition (%)	32.84	10.20	7.02	40.84	1.47	0.26	0.14	0.24	0.78	0.01	1.07

2.1.3 Preparation of Cow Bone (Cb)

The Cb bones were soaked for 24 hours, scraped to remove meat remnants. The bones were boiled in water-detergent at 100 °C for 90 minutes in other to remove fat and oil and thereafter cooled in air as equally reported by Zainal and Hamdzun [14]; Sangeeta et al., [15]; Abdulrahman et al., [16]. The bones were further scrubbed with wire brush in warm water before size reduction by the use of sledge hammer and sun dried for 4 weeks to reduce the moisture [9, 17]. Calcination of the bones were effected in oven (Model SDO/225 with Serial No. Y9C227) at 300 °C for 2 hours to ensure elimination of protein [14, 18]. Denver laboratory ball mill (Model 48-D0500/0 with Serial No. 14002201) was used to crush the bones and pulverized to 75 µm particle size according to BS1377:2014. The chemical composition of cow bone (Table 3) was adopted from Sergius and Janecek [19].

Table 3: Chemical composition of cow bone powder (wt%) [19]

Metal	Ca	Mg	K	P	CO
% Composition	36.05	0.74	0.85	16.43	4.58

2.2 CASTING OF PROPHYLACTIC KNEE BRACE (Pkb) COMPOSITES

2.2.1 Melting and Casting of the Brace

The production of the Pkb aluminium composite was achieved using the stir casting method [12, 20]. The samples were produced by varying the percentage of reinforcing Cb and Ps particles at (1, 2, 4, 6, 8 and 10) wt % of the same 75 μm particle size. The aluminium alloy of mass 292 g was charged into the furnace, which was heated to 850 °C to ensure complete melting of the alloy.

2.2.2 Production of Pkb Composite

In the production of Pkb composite, the furnace temperature was raised to 850 °C and the molten aluminium alloy was allowed to cool in the furnace to a temperature of 700 °C [12]. The Ps was preheated to 200 °C for 1 hour to improve the materials wettability [21]. The preheated Ps was added and stirred for 5 minutes. The composite slurry was re-heated to a temperature of 850 °C and thoroughly stirred for 5 minutes before the melt was poured into a preheated mould with diameter 250 mm and 300 mm length used to prepare cast braces (Figure 3 and 4). The pouring of the melt was maintained at laminar flow to avoid entrapped air. The same procedure was adopted for the casting of Cb aluminium composite with addition of 0.5 wt% Mg for good wettability of particles with molten metal [21].

**Figure 3:** Cast Brace Composite**Figure 4:** Finished Cast Brace Composite

3 RESULTS AND DISCUSSIONS

3.1 Determination of the Density

The density measurements of the samples were carried out using the Archimedes's principle, which states that a body immersed in a fluid is buoyed up by a force equal to the weight of the displaced fluid. The relative density R_D is obtained using equation 1 [20].

$$R_D = \frac{W_a}{W_a - W_w} \quad (1)$$

Where, R_D = Relative density of the composite sample, W_a = weight of the composite in air, W_w = weight of the composite in water.

The density (Figure 5) of the reinforced Ps composites reduced from 2.72 g/cm³ at 1 wt % of Ps addition to 2.60 g/cm³ at 10 wt % of Ps addition. The density of the reinforced Cb composites also reduced from 2.72 g/cm³ at 1 wt % of Cb addition to 2.68 g/cm³ at 10 wt % of Cb addition.

The reduction in density of the cast Pkb was more significant in Ps composites compared to that of Cb composites. The reduction could be because of less dense property of Ps particles as against the Cb particles. The decrease in density with addition of the particulates could be because of the lower density of the fillers compared to that of aluminium metal matrix. This is good because it will enhance the utilization of Al/Ps and Al/Cb metal composites where lighter weight is desired properties. This is in agreement with the work of [12] and [21].

Fig 5 shows the densities of the Al/Ps and Al/Cb composites produced with that of control and original material (OM) used for Pkb. It can be observed that the density of the control and OM is 2.73 g/cm³ and is higher than that of Al/Ps and Al/Cb. The density of Ps reinforced composite is lower compared to the density of Al/Cb, control and OM. The density of Al/Ps composite falls within the range of density of aluminium material used for Pkb.

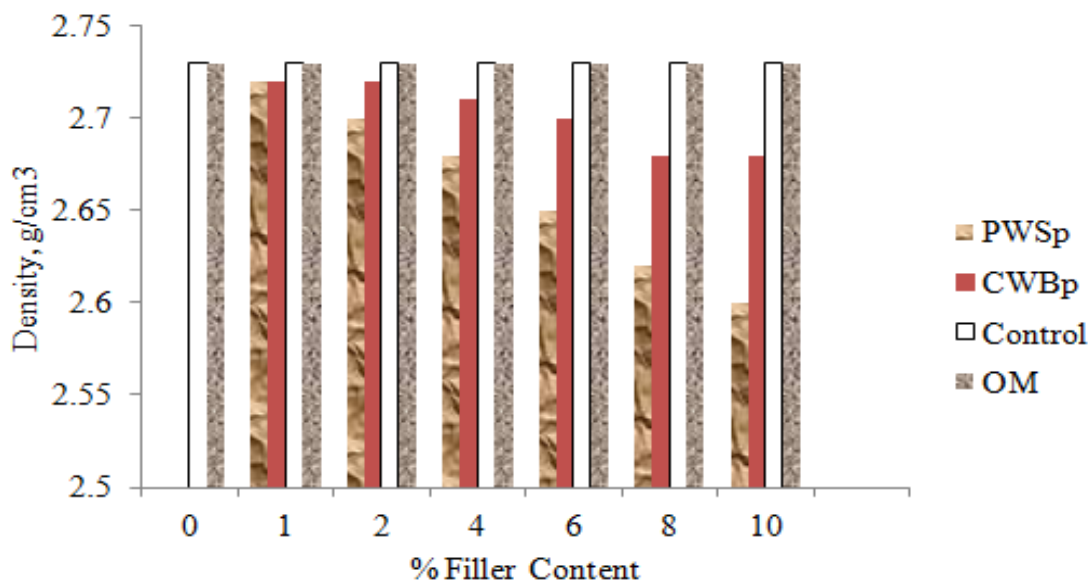


Figure 5: Density of the Al/Ps and Al/Cb composites Vs control sample and OM

3.2 Hardness Property

The hardness properties of the samples (Figure 6) were determined according to ASTM E10 standard procedure using Brinell Hardness Tester (Edibon Brinell Tester, Model EEDB, and Serial No. EEDB0006/13). The machine indenter of diameter 5mm and load 2500N with dwelling time of 15sec was used. According to [22], the average diameter of indentation was used to determine the hardness number of the composites using Equation 2.

$$HB = 0.102 \times \frac{2F}{\pi D(D - \sqrt{D^2 - d^2})} \quad (2)$$

Where, F = Test Force (N), D=Diameter of steel ball (mm), d=Diameter of indentation (mm)

Table 4 shows the hardness values of the produced composites with % wt PwS and % wt Cb, the hardness values of the cast Al/Ps composites increased as the % wt Ps addition increases in the aluminium alloy while that of Al/Cb

initially decreased sharply before steady increases before decreasing. The hardness value of composites increased from 40.30 HBN to 41.80 HBN at 10 wt % addition of Ps. The presence of the hard ceramic phase in the ductile matrix resulted into the increase in the hardness of the Al/Ps composite from 40.50 HBN to 41.80 HBN for 1 wt % and 10 wt % Ps respectively. The Al/Cb composites increased in hardness from 40.10 HBN for 1wt % up until 40.80 HBN for 6 % wt cow bone particles where it gradually decreased to 40.40 HBN at 10 wt % of cow bone particles.

The decrease in hardness of the Cb composite might be due to poor wettability and poor filler dispersion at higher weight fraction and the increments of hardness of Al/Ps was attributed to increase in weight percentage of hard and brittle phase of the Ps particles in the aluminium alloy. The increase in hardness could be due to the effect of the increase in the interfacial contact area between the matrix and the reinforcement.

This hardness experience in the Ps composites is likely to be from SiO₂, Al₂O₃, CaO and Fe₂O₃ present. Figure 6 shows the hardness value recorded for the produced aluminium particulates composites and control as well the OM. It was observed that Al/Ps composites possess the average highest hardness values of 41.18 BHN followed by the Al/Cb composites with 40.45 BHN as compared to control with 40.30 BHN used for Pkb.

Table 4: Hardness values of Al-wt % Ps and Cb knee brace produced

Percentage composition of Al/Ps and Al/Cb		Hardness (BHN)	
		Periwinkle shell	Cowbone
99%	1%	40.50	40.10
98%	2%	40.80	40.30
96%	4%	41.20	40.60
94%	6%	41.30	40.80
92%	8%	41.50	40.50
90%	10%	41.80	40.40

Hardness value of control sample = 40.30
 Hardness value of original material = 40.50

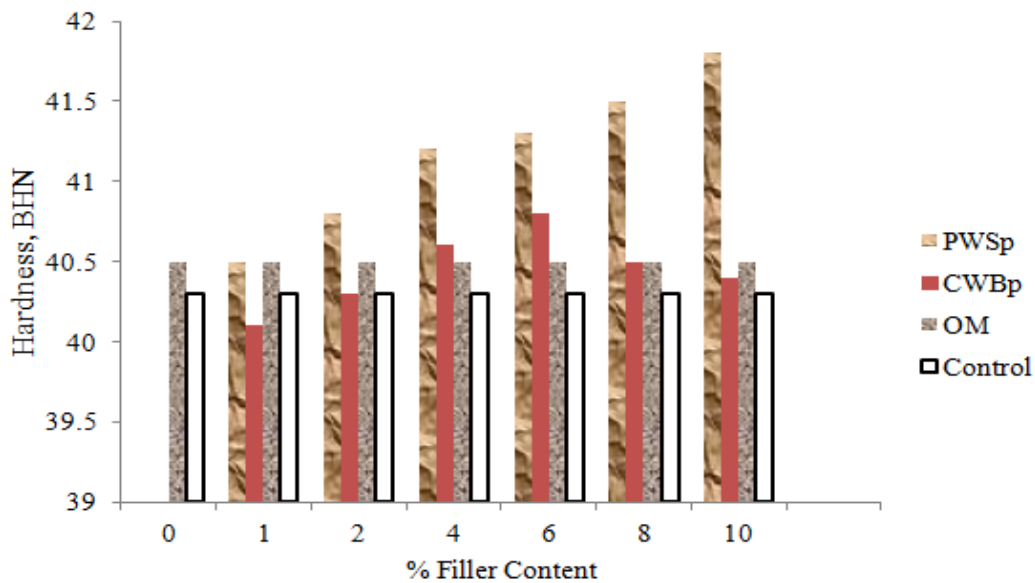


Figure 6: Hardness values for Al/Ps and Al/Cb with Control and OM

3.3 Tensile Strength

The results of the tensile strength (Table 5) revealed that the tensile strength of the aluminium alloy was improved with increasing weight fraction of the reinforcements (Ps and Cb). This was due to the increase in the percentage of Ps and Cb particulates, which is likely to result in production of more calcium silicate giving higher strength in the composite produced. Al/10 wt % Ps samples give more strength (140.30 MPa) while the Al/10 wt % Cb gives strength value of 138.20 MPa which is lower than that obtained from PwS sample, hence Ps impacts more strength in aluminium than the Cb. This result may be attributed to the strengthening effect of the particulates on the aluminium alloy matrix. This behaviour is in agreement with the work of Nwabufor [13], Agunsoye et al, [18] and Aigbodion,

[21]. Figure 7 shows the tensile strength of Al/Ps and Al/Cb composites produced with control and OM. The tensile strength of the control sample is lower compared to that of OM. When the addition of Ps and Cb from 1-10 wt % was made, it was observed that the tensile strength of the aluminium composites increased significantly and had higher values compared to the control and OM.

Table 5: Tensile strength of Al-wt % Ps and Cb knee brace produced

Percentage composition of Al/Ps and Al/Cb	Tensile strength (MPa)	
	Periwinkle shell	Cow bone
99% 1%	131.50	130.90
98% 2%	132.80	131.50
96% 4%	135.70	133.70
94% 6%	136.90	135.90
92% 8%	138.10	137.60
90% 10%	140.30	138.20

Tensile strength of control sample = 130.10 MPa

Tensile strength of OM = 135.17 MPa

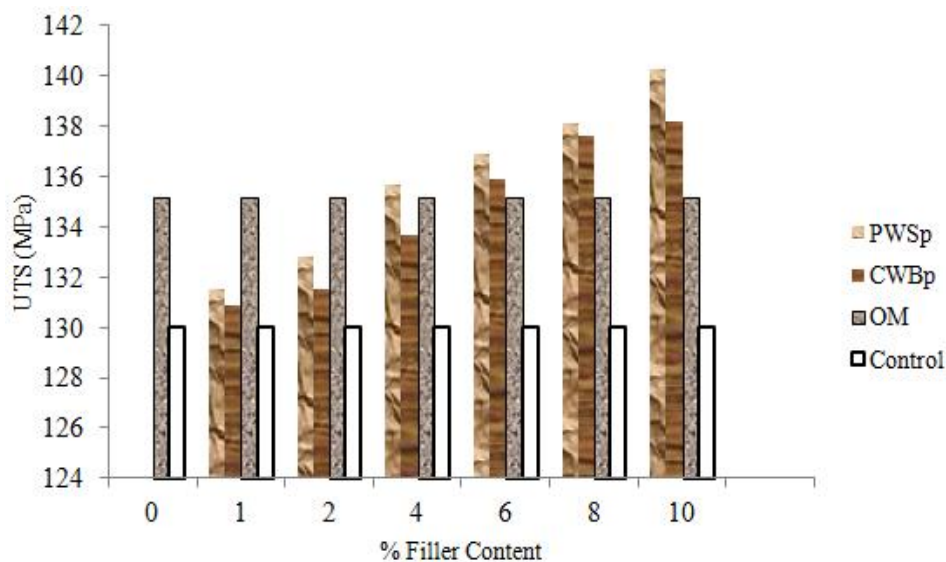


Figure 7: Tensile strength of Al/Ps and Al/Cb with control and OM

4 CONCLUSIONS

Investigation on hardness and tensile properties of prophylactic knee brace produced from cow bone and periwinkle shell composites, using Ps and Cb as reinforcements has been reported. The evaluations of the hardness and tensile properties of the cast aluminium brace, has necessitated the following conclusions:

1. Aluminium composite of lightweight can be produced using Ps and Cb because the density of the produced Al/Ps and Al/Cb composites reduced with increase in the addition of Ps and Cb.
2. The tensile strength of 140.30 and 138.20 MPa were obtained for 90 % cast aluminium base metal matrix composite with 10 % weight percent addition of Ps and Cb particles respectively. The tensile strength of cast aluminium base metal matrix composite increases as weight percent addition of Ps and Cb particles increases.
3. The hardness of the Al/Ps composites increased as the % wt Ps addition increases in the cast aluminium alloy.

FURTHER WORK

Investigation on the impact and buckling properties on the cast Pkb with Ps and Cb particulates as reinforcements is to be carried out.

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